

# Flood Risk Assessment & Drainage Strategy

Title	Land South of A617	
Client	ROMO Holdings Ltd	
Location	Rainworth, NG21 0JY	
Project number	18-0494	
BIM reference	RAIN-BSP-ZZ-XX-RP-C-0001-P04_FRA_DS	
Date	16th March 2021	



# Authorisation Sheet & Revisions Record

Project Number:	18-0494
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Client:	ROMO Holdings Ltd
Location:	Rainworth, NG21 0JY
Document Reference:	CLBR-BSP-ZZ-XX-RP-C-0001-P04_FRA_DS
Office Address:	BSP Consulting, 5 Pride Point Drive, Derby, DE24 8BX
Telephone No:	0115 704 3300

Rev:	Issue Date:	Description:	Prepared:	Checked:	Authorised:
P01	18/12/20	Initial Issue	BJS	MV	MA
P02	20/01/21	Updated to include FPCR latest development framework plan	BJS	MV	MA
P03	04/03/21	Report title amended	BJS	CN	MA
P04	16/03/21	Updated FCPR drawing and site location	BJS	CN	MA

BJS	Ben Seamer	b.seamer@bsp-consulting.co.uk
	MEng, BEng (Hons)	Graduate Civil Engineer
CN	Craig Noonan	m.viggars@bsp-consulting.co.uk
	BSc (Hons)	Principal Civil Engineer
MA	Monika Anszperger	m.ansperger@bsp-consulting.co.uk
	MEng CEng MIStructE	Associate



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# Executive Summary

Introduction	BSP Consulting has been commissioned by ROMO Holdings Ltd to undertake a Flood	
	Risk Assessment and Drainage Strategy for the development of Land South of A617,	
	Rainworth. This Flood Risk Assessment has been prepared in accordance with the	
	Technical Guidance to the National Planning Policy Framework. This report is written in	
	support of an outline planning application for the site.	
Development	The proposals are for the construction of up to 95 dwellings and associated	
Description and	infrastructure.	
Planning Context		
Existing Site	The site is currently a greenfield site with mostly vegetation. There is an existing wetland	
Conditions	within the east of the site as well as Rainworth Water which runs south to east towards	
	the east of the site. An existing dismantled railway runs through the site parallel with the	
	south western boundary which is to be retained. The site slopes west at a maximum	
	existing level of approximately 101.560mAOD to east at a minimum level of 87.16mAOD.	
Definition of Flood	Rainworth Water and adjacent wetland runs through the east of the site from south to	
Hazard	north. Fluvial flooding and ground water flooding are not considered as significant risks	
	to the site. Surface water flooding is the primary concern on the development site.	
Probability	The EA Risk of Flooding from Rivers and Sea mapping indicates that the proposed site	
(Rivers/fluvial)	has a less than 0.1% (1:1000 year) probability of flood event occurring due to flooding	
	from any local watercourses. An area to the east of the site is at 0.1%-1% chance of	
	flooding due to the existing wetland.	
Climate Change	The implications of climate change of up to 40% are to be considered in the assessment	
	of surface water drainage, with the mitigation measures being determined accordingly.	
	The site lies entirely in Flood Zone 1 so fluvial climate change effects have not been	
	considered.	
Development	In accordance with NPPF, the residential use in Flood Zone 1 falls under the more	
Proposals	vulnerable category in terms of flood risk. The proposed development site is located	
	mostly in Flood Zone 1.	



Flood Risk	The site is at some risk surface water flooding. Floor levels should therefore be set a		
Management	minimum 600mm above the equivalent 1:100yr+40% CC flood plain levels of the existing		
Measures	wetland. Finished floor levels should also be set 150mm above external surrounding		
Measures			
	areas to mitigate problems caused by localised surface water ponding.		
Off Site Impacts	The proposed development drainage will discharge via soakaways or discharge will be		
	limited to greenfield rates of 4.75l/s/ha. Attenuation via open suds features would appear		
	to be viable and is to be accommodated within a future detailed scheme layout. The		
	Rainworth Heath SSSI is located approximately 0.1km downstream of the site. The		
	inclusion of SuDS features and flow controls within the proposed drainage strategy will		
	ensure that water is treated and discharged at a controlled rate such that there are no		
	adverse effects to Rainworth Heath SSSI. The proposed development will therefore not		
	increase or exacerbate any flooding problems adjacent to or downstream of the site.		
Residual Risks	The investigations carried out as part of this flood risk assessment and flood risk		
	management measures proposed have demonstrated that the development will be safe,		
	without increasing flood risk elsewhere.		
Recommendations	The following recommendations are made to ensure flood risk at this site is minimised:		
	• The proposed surface water drainage system should be designed to		
	accommodate the 1 in 30-year rainfall event without any surface water flooding		
	and should be capable of retaining the 1 in 100 year plus climate change storm		
	event of + 40% on site without flooding any buildings.		
	<ul> <li>Floor levels should be set a minimum 600mm above the 1% flood plain levels</li> </ul>		
	of 88.310mAOD. i.e a minimum floor level of 88.910mAOD.		
	• The floor levels should however be set a minimum of 150mm above the		
	surrounding external levels in line with general good practice to mitigate any		
	potential adverse effects as a result localised surface water ponding.		
	<ul> <li>Site topography favours a surface gravity sewage layout. The discharge options</li> </ul>		
	are as follows:		
	- Discharge via soakaways subject to ground investigations.		
	-Discharge to Rainworth Water. Open water storage to be provided. Discharge		
	rates are to be restricted by flow control(s). Total discharge rate should be		
	limited to greenfield rates of 4.75l/s/ha.		
	<ul> <li>A new foul connection is proposed to the public combined sewer running south</li> </ul>		
	to north through the east of the site.		
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# 1.0 Introduction

# 1.1 Terms of Reference

- 1.1.1 BSP Consulting has been commissioned by ROMO Holdings Ltd to undertake a Flood Risk Assessment and Drainage Strategy for the development of Land South of A617, Rainworth. This Flood Risk Assessment has been prepared in accordance with the Technical Guidance to the National Planning Policy Framework.
- 1.1.2 This Flood Risk Assessment has been prepared in accordance with the Department for Communities and Local Government (DCLG) Planning Practice Guidance website section on 'Flood Risk and Coastal Change' and the Site-Specific Flood Risk Assessment Checklist.
- 1.1.3 This report is written in support of an outline planning application for the site.
- 1.1.4 This report has been produced on behalf of the client, ROMO Holdings Ltd, and no responsibility is accepted to any third party for all or any part. This report should not be relied upon or transferred to any other parties without the express written authorisation of BSP Consulting. If any unauthorised third party comes into possession of this report, they rely on it at their own risk and the authors owe them no duty of care or skill.

# 1.2 **National Planning Policy Framework**

- 1.2.1 The National Planning Policy Framework (NPPF) was published on 27 March 2012, with the latest update published in February 2019. This replaces Planning Policy Statement 25: Development and Flood Risk.
- 1.2.2 Planning Practice Guidance to the NPPF regarding Flood Risk and Coastal Change has been published and this site-specific FRA is written in compliance with this guidance.
- 1.2.3 The NPPF, and supporting technical guidance, can be downloaded free of charge from the internet at the following link:

http://www.communities.gov.uk/publications/planningandbuilding/nppf

# 1.3 Legislation/Guidance Background

- 1.3.1 In line with the Building Regulations Part H and Ciria SuDS Manual C753 the site should follow the "Hierarchy of SuDS". This states that the primary means of drainage for any development site should be to the ground (via infiltration). Where this not feasible discharge should be made to a nearby watercourse, only if both of these options are not possible should discharge to sewerage systems be made.
- 1.3.2 The drainage systems themselves should be designed to enable adoption by an appropriate authority or recognised body to ensure ongoing maintenance is provided.



- 1.3.3 New Ofwat codes for adoptable sewers came into force in England from April 2020 replacing all versions of Sewer for Adoption. This new guidance *"Design and Construction Guidance for foul and surface water sewers"* (DCG) is for use by developers when planning, designing and constructing foul and surface water drainage systems intended for adoption by English water and sewage companies under a section 104 agreement. It differs from the outgoing Sewers for Adoption guidance as compliance will be mandatory.
- 1.3.4 The adoption code is significant as it provides the mechanism by which water companies can secure the adoption of a wide range of SuDS components that are compliant with the document. It is noteworthy that the water companies are yet to publish their addendum documents to set out what criteria will be used to determine what constitutes "compliant". It is, however, widely expected that this will make strong reference to C753, see section 1.3.1 above.
- 1.3.5 The new code states that the layout of the whole development including the drainage layout should be considered at the earliest stages of the design as it is fundamental to the performance and affordability of the drainage system as well as the wider urban design including the character of the development, amenity, biodiversity, connectivity and use of the site.
- 1.3.6 Other key points in relation to the design and construction of new surface water drainage systems include:
  - The location of adoptable drainage components should take account of the need to provide appropriate access to each component for maintenance.
  - Health and safety risks should be assessed and managed in accordance with Ciria C753 SUDS manual and a copy of the principle designers risk assessment submitted to the water company.
  - Provided there is provision for the flows to reach a particular feature, surface SuDS features designed to take 1 in 100 year rainfall event plus climate change will normally be adoptable.



# 2.0 Background Information

# 2.1 Site Details

2.1.1 Figure 2.1 below indicates the location of the site; a more detailed site plan is located in **Appendix A**. A range of sources have been used to assess the local topography, local watercourses and current site use.



Figure 2.1 Land South of A617, Rainworth - Site Location Plan

2.1.2 The proposed development site boundary is indicated by the red outline, occupying approximately 6.6ha.It is located to the south of A617 centred at approximately OSNGR 459050 E, 358650 N.



- 2.1.3 The site is currently a greenfield site with mostly vegetation. There is an existing wetland within the east of the site as well as Rainworth Water which runs south to east towards the east of the site. An existing dismantled railway runs at an elevated level through the site parallel with the south western boundary and is to be retained The site is bounded by A617 Rainworth bypass towards the northeast; Hedge and vegetation towards north west; Rufford Colliery Way and vegetation towards the east and gardens to existing lots towards the south of the site.
- 2.1.4 A survey was carried out to assess the topography of the site and is included in **Appendix B.** The site slopes west at a maximum existing level of approximately 101.560mAOD to east at a minimum level of 87.16mAOD.

Classification	Name	Description
Main Rivers	N/A	There are no main rivers in close located in close proximity to the site.
Ordinary Watercourses	Rainworth Water	Rainworth Water runs enters the site along the south west boundary and approximately runs south to north.
	Unknown	There is an existing pond/wetland located towards the east of the site.
Canals	N/A	There are no live Canals located in close proximity to the site.
Riparian Watercourses	N/A	There are no riparian watercourses located in close proximity to the site

# Table 2.1: Overall Catchment Context and Local Watercourse Classifications

2.1.5 The approximate locations of the above watercourses are indicated on Figure 2.1 above.

# 2.2 Approach to the Assessment

- 2.2.1 Publicly available online Environmental agency (EA) flood mapping has been used to assess flood levels for the site and local area. Correspondence with the Lead Local Flood Authority (LLFA) is also referred to in the report.
- 2.2.2 This study has been supplemented by additional information from Severn Trent Water (STW), information contained on the British Geological Society (BGS) website and site Investigation works by GeoDyne.
- 2.2.3 This assessment seeks to draw together the relevant level information from the EA and to collate this with the findings of our investigations and discussions to assess the flood risk at this site.



# 3.0 Flood Risk Assessment

# 3.1 Development Description and Planning Context

- 3.1.1 The proposals are for the construction of up to 95 dwellings and associated infrastructure
- 3.1.2 A proposed site concept layout is included as **Appendix A**.
- 3.1.3 In accordance with NPPF, the residential use falls under the **more vulnerable** category in terms of flood risk.

# 3.2 **Definition of Flood Hazard**

The potential sources of flooding in the vicinity of the site are as detailed below:

# **Fluvial Flood Risk**

3.2.1 The site is not located in close proximity to any main rivers or live canals. Rainworth Water runs along the western boundary of the site.



Figure 3.1 Land South of A617, Rainworth – Fluvial Flood Mapping

3.2.2 Figure 3.1 shows the site majority of the site is located in Flood Zone 1 with less than 0.1% chance of flooding from fluvial sources. There is an area of the site considered as being at 0.1%-1% chance of flooding from existing wetland.



- 3.2.3 As the majority of the proposed development site is located entirely in Flood Zone 1 and the proposed residential development is not proposed within the area considered as being in Flood zone 2, it does not require sequential or exceptions testing.
- 3.2.4 The flood risk associated with the existing wetland and Rainworth Water is considered further in the surface water flood risk section. Hence, the site is not considered as being at significant risk of fluvial flooding.

# **Tidal Flood Risk**

High 🌑 Medium 🔵 Low (

) Very low

3.2.5 The site is not located in close proximity to any tidal rivers or seas. The lowest point of the site is approximately 87.16mAOD and is therefore not at risk of flooding from tidal sources.

# <image>

# Surface Water Flood Risk

Figure 3.2 Land South of A617, Rainworth – Surface Water Flood Mapping

- 3.2.6 Figure 3.2 above shows that majority of the site is at very low risk of surface water flooding. An area towards the eastern part of the site has a low to high (0.1%-3.33%) probability of flooding due to surface water. Surface water flooding, delivered by the wetland adjacent to Rainworth Water, is therefore considered as the primary concern flooding to the site.
- 3.2.7 The natural topography of the site also suggests that the east of the site may be at risk of pluvial flooding.



# Flood Risk from Ground Water

- 3.2.8 The British Geological Survey's Geology of Britain mapping indicates that the site is situated upon bedrock geology of Chester Formation consisting of Sandstone, Pebbly Sedimentary rock. No Superficial Deposits.
- 3.2.9 The bedrock is classed as a Principal aquifer on DEFRA mapping.
- 3.2.10 Any risk associated with this source is likely to be influenced by the local watercourses. If groundwater flooding was to occur, this would likely be due to heavy rainfall and standing water and any resulting groundwater flooding would occur in conjunction with surface water flooding.
- 3.2.11 Subject to Phase I & II ground investigations, ground water flooding can be discounted as a considerable source of flood risk to the site.

# Flood Risk from Sewers and Infrastructure

- 3.2.12 The Environmental Agency mapping confirms that the site does not lie in an area that is at risk of flooding from reservoirs.
- 3.2.13 The site is not within close proximity of any wet process industrial works.
- 3.2.14 An existing 750Ømm combined sewer runs approximately south to north through the east of the site.
   STW developer enquiry response indicates foul flows from the proposed site can be accommodated in this 750Ømm sewer and hence is not considered as a significant risk of flooding to the site. See Appendix
   D for sewer location and STW developer enquiry response. It is sat within the lower area of the site and should any flooding occur this would not impact the development areas.
- 3.2.15 STWL have been consulted regarding the development proposals and have not raised any concerns regarding any potential for flooding or drainage capacity issues. A copy of the STWL Development Enquiry and other correspondence are included in **Appendix D**.
- 3.2.16 The sewers and infrastructure flood risk source can therefore be discounted as a significant source of flood risk to the site.

# 3.3 **Probability of Flood Risk**

3.3.1 Publicly available flood mapping indicates that the majority of the site is at less than 0.1% probability of flooding due to fluvial and surface water sources. An area to the east of the site is at 0.1%-3.33% chance of flooding due to surface water flooding. This map shows the indicative extent of the natural floodplain, if there were no flood defences or certain other manmade structures, such as surface water sewers, and channel improvements.



# 3.4 Climate Change

- 3.4.1 Climate change is recognised as a factor for consideration in terms of its effects on flood risk. However, the site is within flood zone 1 so climate change factors do not need to be considered in terms of fluvial flooding.
- 3.4.2 The implications of climate change should be taken into account in relation to surface water drainage. Peak rainfall intensity for longer lifetime residential developments is estimated to increase between 20% and 40% as a result of climate change. In this instance the site is in close proximity to Rainworth Water and has a 0.1% - 3.33% probability of flooding due to surface water. Therefore, it is recommended that the Upper End allowance of 40% is applied to design rainfall intensity to allow for the potential implications of climate change. This is in line with the LLFA planning request.

# 3.5 **Detailed Development Proposals**

- 3.5.1 The proposed development and vulnerability classification are discussed in **section 3.1** above and the proposed site is included within **Appendix A**.
- 3.5.2 In accordance with the NPPF, the proposed residential use falls under the more vulnerable category in terms of flood risk. The proposed development site is located mostly in Flood Zone 1.

# 4.0 Flood Risk Management

# 4.1 Fluvial and Surface Water Flood Risk Mitigation - Finished Floor Levels

- 4.1.1 As outlined in section 3.2, the site is at risk of surface water flooding towards the east of the site. These flood levels have been sketched onto the existing site topography as shown in Appendix E. Assessing the topography alongside the EA flood mapping, it is evident that the flood modelling shown in section 3.2 is not necessarily a true representation of flood levels. The dismantled railway is at an elevated bank level running parallel with the southwestern boundary and is to be retained as part of the development proposals.. The flood mapping currently shows the railway towards the south of the site to be within the 1 in 30-year flood plain. However, since the railway is at an elevated level of 99.13mAOD compared to Rainworth Water top of bank level of 89.36mAOD approximately 15m to the southeast of the railway bank, the flood mapping is considered incorrect in this area.
- 4.1.2 The elevated railway is not reflective of the natural landscaping of the site. Assessing the ground levels further, the first location along the east of the site considered as representative of the natural landscape is approximately the mid point of the eastern boundary of the site. The 1% flood level at this location is approximately 88.310mAOD as noted on the drawing presented in **Appendix E**



- 4.1.3 Due to the uncertainty of flood levels and the consideration for climate change, floor levels should therefore be set a minimum 600mm above the equivalent 1% flood plain levels of 88.310. i.e., a **minimum FFL of 88.910mAOD**.
- 4.1.4 Where practicable, floor levels should also be set a minimum 150mm above surrounding external levels to minimise the risk of surface water flooding due to localised ponding. Where possible, levels should also be set as to create gradients which fall away from housing plots.

# 4.2 Surface Water Drainage

# Sustainable Drainage Systems

- 4.2.1 Part H of the Building Regulations 2010 recommends that surface water run-off shall discharge to one of the following, listed in order of priority:
  - a) an adequate soakaway or some other adequate infiltration system, or where that is not reasonably practicable.
  - b) a watercourse, or, where that is not reasonably practicable.
  - c) a sewer.
- 4.2.2 It is necessary to identify the most appropriate method of controlling and discharging surface water. The design should seek to improve the local run-off profile by using systems that can either attenuate run-off and reduce peak flow rates or positively impact on the existing flood profile.

# Discharge via Infiltration Based Systems

- 4.2.3 Ground investigations have not yet been undertaken for the site. In line with the hierarchy of SuDS the option to discharge via soakaways should be explored first subject to ground conditions.
- 4.2.4 Regional mapping suggests soakaways may be viable, refer to section 3.2.8, however the presence of the wetland to the east of the site would appear to contradict this slightly.
- 4.2.5 Should infiltration drainage prove viable it must provide the main means of draining the development, features such as infiltrating swales, plot soakaways and a highway infiltration basin should be considered. It is noted that these features will require no further space beyond those proposed in the non-infiltrating scenario, as such the worst case, non-infiltrating scenario, has been considered through-out the remainder oof the report.

# **Discharge via Open Watercourses**

4.2.6 Should the option to discharge via soakaways be found to not be practicable, Rainworth water to the east of the site provides a suitable watercourse to discharge to. This is in line with LLFA planning request included in **Appendix C**.



- 4.2.7 The proposed drainage design should aim to limit the new surface water discharge rate to Qbar, as set out in the NCC LLFA planning response. See **Appendix C**.
- 4.2.8 In the case where surface water is to discharge to Rainworth Water, surface water attenuation is to be provided open water storage. The attenuation is to be coupled with flow control(s) to limit the total surface water discharge into the watercourse to QBar greenfield rates as requested by the LLFA. The proposed drainage layout outline showing approximate attenuation to outfall locations to the brook is included in Appendix E. LLFA correspondence confirming the allowable discharge rate is included in Appendix C.
- 4.2.9 Preliminary surface water attenuation calculations have been made based on the following figures:
  - Total site area of 6.6ha. Qbar for total site= 31.49l/s. This (see **Appendix F** for calculations)
  - A total of approximately 4.4ha is determined as developable land.
  - 60% of the developable land is assumed impermeable.
  - Approximate total impermeable catchment area for the site of 2.64ha.
- 4.2.10 The total discharge rate cannot exceed 31.49/s, equating to approximately 4.75l/s/ha. However formal discharge is to be based upon the developed area only, discounting any open space. Based upon a 60% impermeable rate of the developable land at a rate of 4.75l/s/ha, the total design site discharge is expected to be 12.6/s.
- 4.2.11 It is noted that the QBar figure derived in calculations is as a result of a manual edit of the soil parameters in the greenfield run-off calculator. The un-adjusted calculator results suggest a very low QBar figure, in line with regional mapping. However for the purposes of testing the masterplan it has been taken that the site is not suitable for infiltration.
- 4.2.12 Quick storage estimates have been carried out to assess the attenuation requirements and discharge rates. The storage requirements are summarised as follows:

Total Catchment Area	2.64ha
Discharge Rate	12.6 l/s
Storage Required	1711-2300m <sup>3</sup>

Table 4.1 Attenuation Requirements

- 4.2.13 A copy of the quick storage estimate results is included in **Appendix G**.
- 4.2.14 Attenuation is to be provided through a combination of a pond and swales across the site. Indicative locations for these storage features are shown in **Appendix E.**



4.2.15 Following the introduction of the DCG in Oct 2019 the SUDS pond design can now be presented to STWL for consideration of adoption such that they own and maintain it along side their transitional piped system.

# **Discharge via Sewers**

- 4.2.16 STWL developer enquiry response indicated public sewers are present through the site. A copy of the developer enquiry is included in **Appendix D**.
- 4.2.17 However, due to the site topography and close proximity to Rainworth Water (allowing for discharge into an existing watercourse), it is not currently proposed to discharge surface water into public sewers.

# 4.3 **Design Consideration of Exceedance**

- 4.3.1 The proposed surface water drainage system should be designed to accommodate the 1 in 30-year rainfall event without any surface water flooding and should be capable of retaining the 1 in 100 year plus climate change storm event of + 40% on site without flooding any buildings. The depth of the flood water should be considered in detailed design to ensure that they do not pose a hazard on site.
- 4.3.2 In the event of a failure of the existing drainage system, flood flow routes through the proposed development should be included at the detailed design stage. This will require consideration of the proposed finished floor and external levels, such that potential flood waters can flow away from the site with the local topography without entering the proposed or existing buildings.

# 4.4 Residual Risks & Off-Site Impacts

- 4.4.1 The proposed development drainage discharge will be limited to Qbar greenfield rates of 4.75l/s/ha, as discussed in section 4.2.7. Therefore, the proposed development will not increase or exacerbate any flooding problems adjacent to or downstream of the site.
- 4.4.2 The Rainworth Heath SSSI is located approximately 0.1km downstream of the site. The inclusion of SuDS features and flow controls within the proposed drainage strategy discussed previously will ensure that water is treated and discharged at a controlled rate such that there are no adverse effects to Rainworth Heath SSSI.
- 4.4.3 The investigations carried out as part of this flood risk assessment and flood risk management measures proposed have demonstrated that the development will be safe, without increasing flood risk elsewhere.

# 4.5 **Foul Water Discharge**

- 4.5.1 Local sewers are operated and maintained by STWL. The initial developer enquiry indicates that there is a 750mmØ combined water gravity sewer running through the site south to north and has the capacity to accommodate the foul flows generated by the proposed site. STW sewer records are shown in **Appendix** 
  - D.



- 4.5.2 It is therefore proposed that the sites foul water discharges into the existing 750mmØ public combined sewer subject to STW S106 approval. Correspondence with STW approval for discharge is included in Appendix D.
- 4.5.3 STW have advised that the existing combined water sewers running through the site require a 10m easement across the site.

# Recommendations

The following recommendations are made to ensure flood risk at this site is minimised:

- The proposed surface water drainage system should be designed to accommodate the 1 in 30year rainfall event without any surface water flooding and should be capable of retaining the 1 in 100 year plus climate change storm event of + 40% on site without flooding any buildings.
- Floor levels should be set a minimum 600mm above the 1% flood plain levels of 88.310mAOD.
   i.e a minimum floor level of 88.910mAOD.
- The floor levels should however be set a minimum of 150mm above the surrounding external levels in line with general good practice to mitigate any potential adverse effects as a result localised surface water ponding.
- Site topography favours a surface gravity sewage layout. The discharge options are as follows:

- Discharge via soakaways subject to ground investigations.

-Discharge to Rainworth Water. Open water storage to be provided. Discharge rates are to be restricted by flow control(s). Total discharge rate should be limited to greenfield rates of 4.75l/s/ha.

• A new foul connection is proposed to the public combined sewer running south to north through the east of the site.

# Disclaimer

We would note that all comments made in this report are based on the sources stated in Section 1.1. This report and its recommendations are intended for the use of ROMO Holdings Ltd for the above site only.



# Appendix A

FPCR Site location 9474-L-07

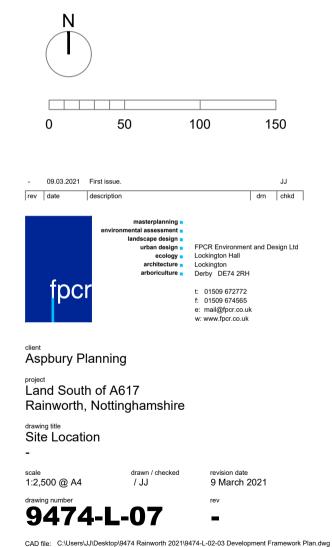
FPCR Development Framework 9474-L-02A

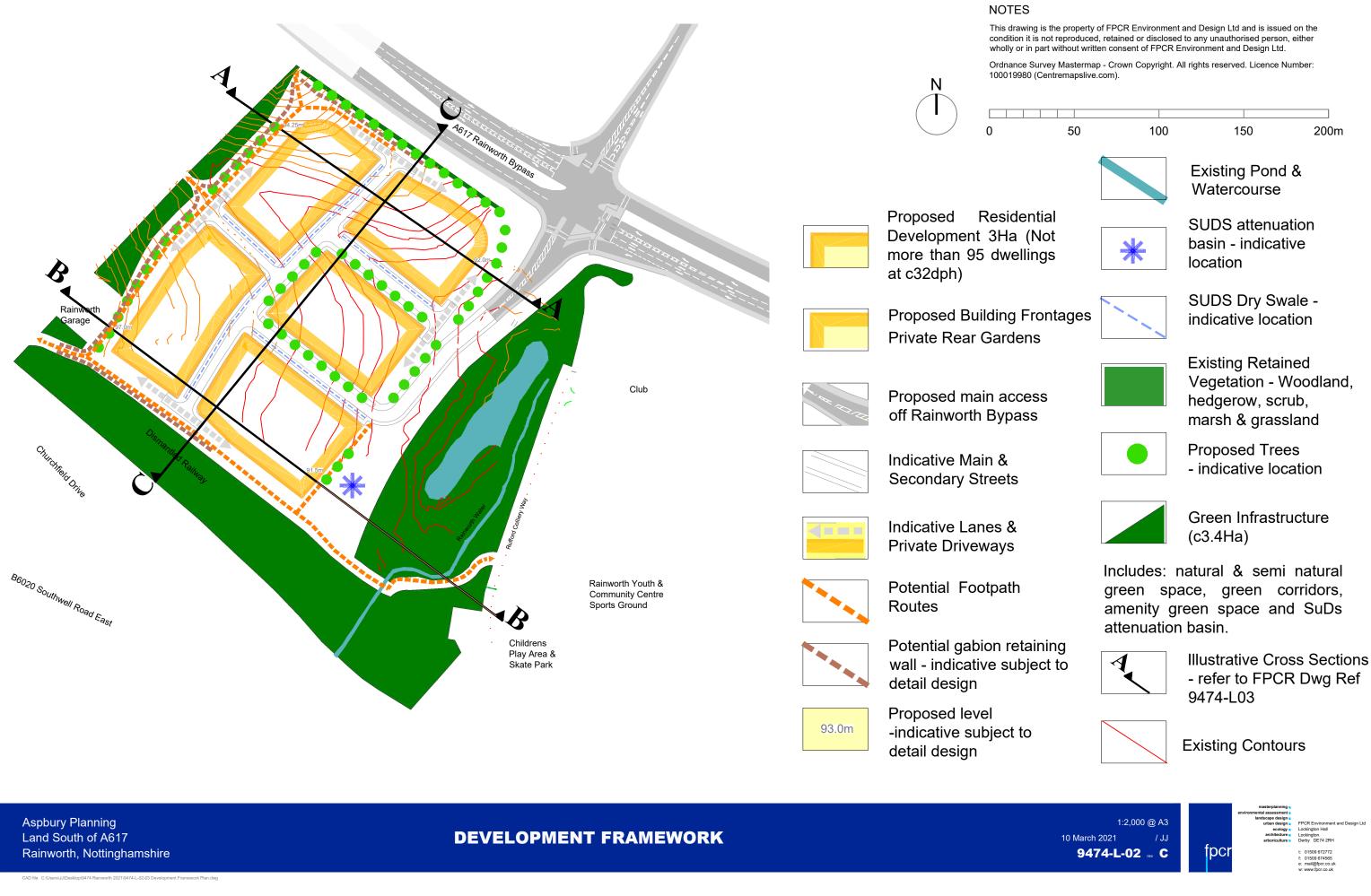


# NOTES

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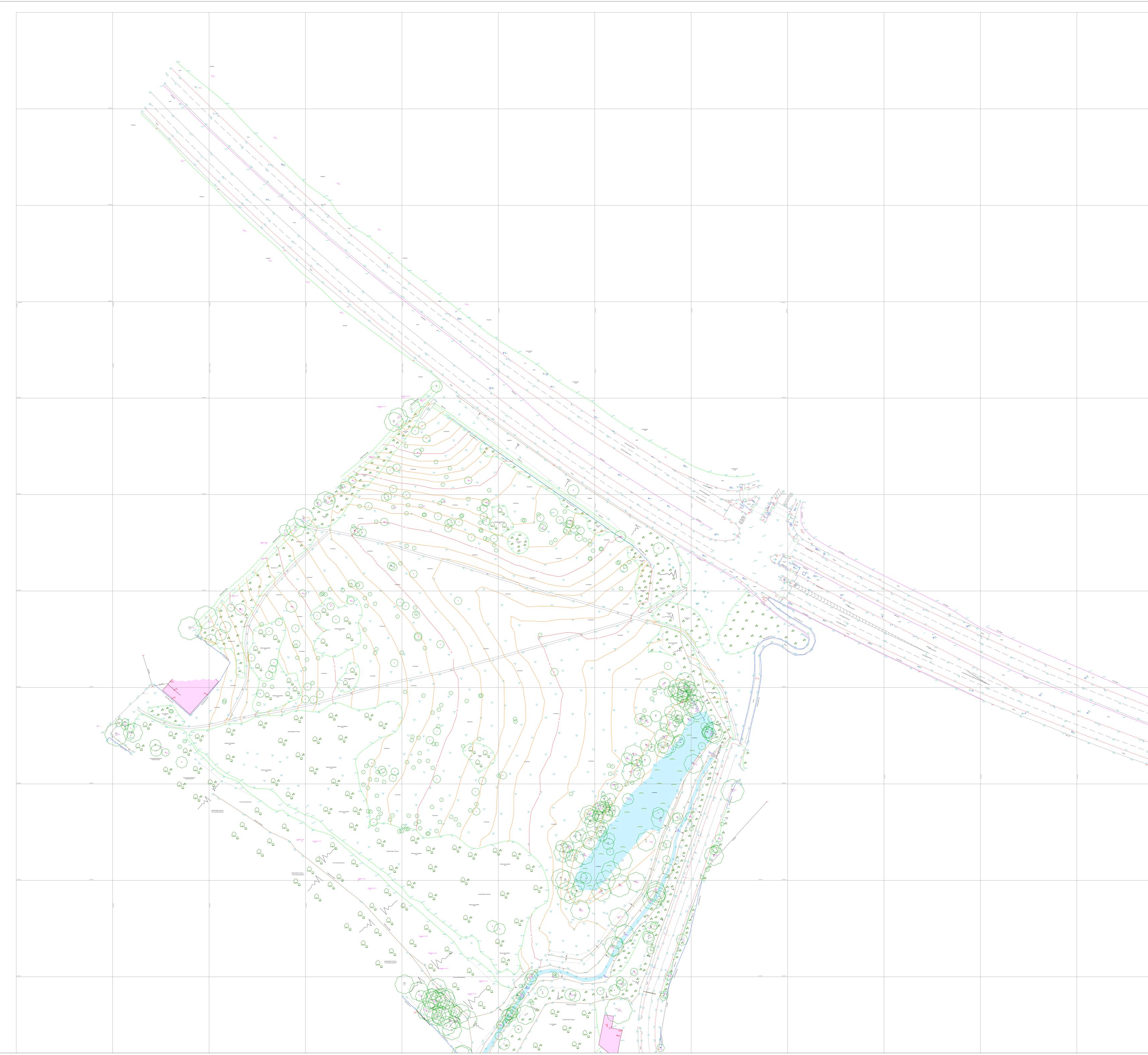




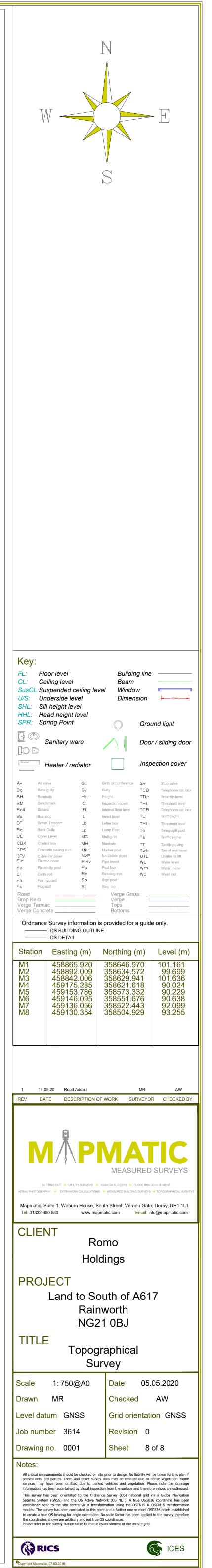


# Appendix B

Mapmatic Topographical Survey 3614\_Rev 1A



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	342704	
	3080X	
	Gons Baken 200 Gons Cons Cons	
1000 1000 1000 1000 1000 1000 1000 100		





# Appendix C

LLFA Response

# **Ben Seamer**

From:	Ross Marshall <ross.marshall@nottscc.gov.uk></ross.marshall@nottscc.gov.uk>
Sent:	09 April 2020 12:26
То:	Ben Seamer
Subject:	RE 18-0494 Rainworth

Hi Ben

I've copied below our standard expectations from a surface water design and trust these help.

"Given the proposed scale of the development to satisfy the National Planning Policy Framework (NPPF) further details would need to be submitted to support this application. Paragraph 163 fn.50 of the NPPF requires that applications in Flood Zone 2, 3 and in Flood Zone 1 over 1 hectare should be accompanied by a site-specific flood risk assessment, reviewing the potential flood risks to the development from all sources. An FRA is vital if the local planning authority is to make an informed planning decision.

As LLFA we also require details of the proposed surface water drainage strategy for the development. Paragraph 165 of the NPPF states that major developments should incorporate sustainable drainage systems unless there is clear evidence that this would be inappropriate. The LLFA advise that any proposed drainage strategy should be in accordance with CIRIA C753 and current best practice guidance. Any FRA or drainage strategy should include following information:

- With regards to an acceptable surface water management scheme for the site we would offer the following comments and recommendations;
  - Provide evidence of a proven outfall from site in accordance with the drainage hierarchy the follows options should be considered, in order of preference; infiltration, discharge to watercourse, discharge to surface water sewer or discharge to combined sewer.
  - Justification should be provided for the use or not of infiltration, including the results of soakaway testing, in accordance with BRE 365.
  - The maximum discharge should be set to the QBar Greenfield run-off rate for the positively drained area of development.
  - The site drainage system should cater for all rainfall events up to and including the 1 in 100-year event including a 40% allowance for climate change.
  - For all exceedance to be contained within the site boundary without flooding any properties in a 1 in 100year+CC storm.
  - SuDS systems should be incorporated into the surface water management scheme for the site, preference should be given to above ground SuDS which provide multifunctional benefits.
  - Details of who will manage and maintain all drainage features for the lifetime of the development will be required prior to construction.

This is only a brief outline of the minimum information we would be expecting to see and not an exhaustive list.

# Informative

1. SuDS involve a range of techniques and SuDS methods can be implements on all sites. SuDS are a requirement for all major development as set out within paragraph 165 of the NPPF.

- 2. The LLFA does not consider oversized pipes or box culverts as sustainable drainage. Should infiltration not be feasible at the site, alternative sustainable drainage should be used, with a preference for above ground solutions.
- 3. Surface water run-off should be controlled as near to its source as possible through a sustainable drainage approach to surface water management. Sustainable Drainage Systems (SuDS) are an approach to managing surface water run-off which seeks to mimic natural drainage systems and retain water on-site as opposed to traditional drainage approaches which involve piping water off-site as quickly as possible. "

Ross Marshall Principal Flood Risk Management Officer 0115 9774473

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# Appendix D

Severn Trent Water Correspondence

# WONDERFUL ON TAP



Severn Trent Water Ltd Leicester Water Centre Gorse Hill Anstey Leicester LE7 7GU

Tel: 02477 716843 www.stwater.co.uk net.dev.east@severntrent.co.uk

Contact: Belal Ali

Our ref: 8406733

BSP Consulting Ltd 5 Pride Point Drive Pride Park Derby DE2

F.A.O: Ben Seamer

5<sup>th</sup> May 2020

Dear Sir/Madam,

# Proposed Development: (70 mixed dwellings) — Land South of A617, Rainworth – 459040 358665

I refer to your Development Enquiry Request in respect of the above site. Please find enclosed the sewer records that are included in the fee together with the Supplementary Guidance Notes (SGN) referred to below.

# Public Sewers in Site – Required Protection

Records show 750mm combined sewer running through site boundary, this pipe will require 10m protection strip, 5m on each side from the pipe centreline. The 300/375mm combined sewer would require same protective strip as above.

Due to the critical nature of this sewer and close proximity to the watercourse any diversion works would be carried out strictly under STW engineering scheme funded by the developer. We would expect the above protective strip to be accommodated at this early stage to avoid a costly diversion. Note diversion schemes can take 18-20 months deliver.

Due to a change in legislation on 1 October 2011 there may be former private sewers on the site which have transferred to the responsibility of Severn Trent Water Ltd, which are not shown on the statutory sewer records, but are located in your client's land. These sewers would require protective strips of 3 metres either side of the sewer's centreline that we will not allow to be built over. If such sewers are identified to be present on the site, please contact us for further guidance.

# Foul Water Drainage

Records show the 750mm combined sewer running within your site boundary is the most suitable connection point for your development. Gravity flows from 70 dwelling can be accommodated in this network. A connection is therefore acceptable subject to a formal S106 submission (see later).

# Surface Water Drainage

Under the terms of Section H of the Building Regulations 2000, the disposal of surface water by means of soakaways should be considered as the primary method. If these are found to be unsuitable, satisfactory evidence will need to be submitted. The evidence should be either percolation test results or by the submission of a statement from the SI consultant (extract or a supplementary letter).

In presence of available watercourse no surface shall discharge to the public network.

Subject to the above, Severn Trent Water expects all surface water from the development to be drained in a sustainable way to the nearest watercourse or land drainage channel, subject to the developer discussing all aspects of the developments surface water drainage with the Local Lead Flood Authority (LLFA). Any discharge rate to a watercourse or drainage ditch will be determined by the LLFA / EA.

# **Connections**

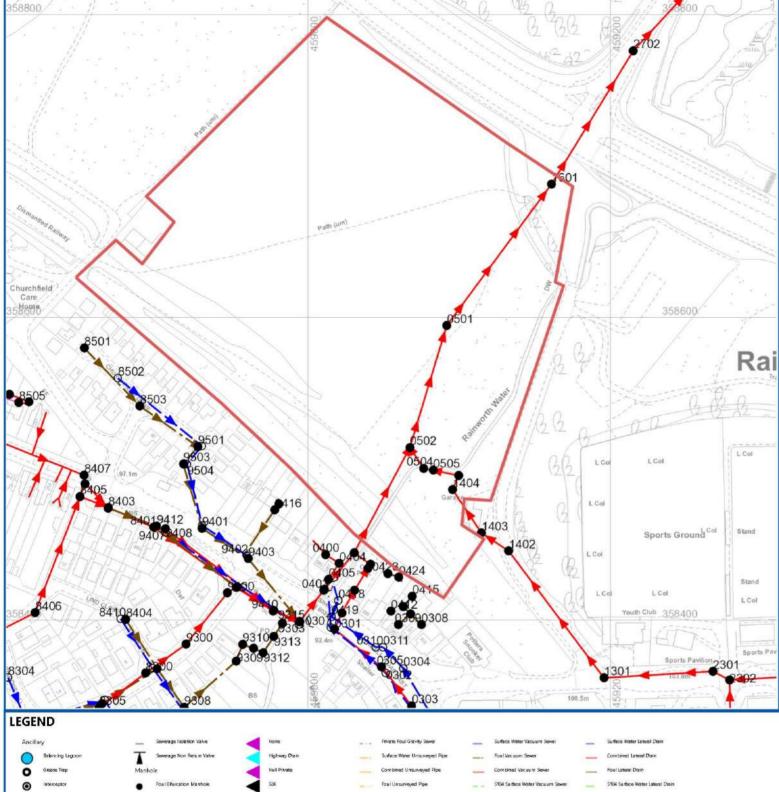
For any new connections (including the re-use of existing connections) to the public sewerage system, the developer will need to submit a Section 106 application form. Our Developer Services department are responsible for handling all new connections enquiries and applications. To contact them for an application form and associated guidance notes please call 0800 7076600 or download from <u>www.stwater.co.uk</u>.

Please quote the above reference in any future correspondence (including e-mails) with STW Limited. Please note that Developer Enquiry responses are only valid for 6 months from the date of this letter.

Yours sincerely

0

Belal Ali Asset Protection Waste Water East Wholesale Network Control and Asset Management



Reference	Cover Level	Invert Level Upstream	Invert Level Downstream	Purpose	Material	Pipe Shape	Max Size	Min Size	Gradient	Year Laid
SK58589309	<unk></unk>	<unk></unk>	<unk></unk>	F	<unk></unk>	С	150	<unk></unk>	0	31/12/1899 00:00:00
SK58589313	<unk></unk>	<unk></unk>	<unk></unk>	F	<unk></unk>	С	150	<unk></unk>	0	31/12/1899 00:00:00
SK58589311	<unk></unk>	<unk></unk>	<unk></unk>	F	<unk></unk>	С	150	<unk></unk>	0	31/12/1899 00:00:00
SK58588311	93.86	92.65	91.38	S	<unk></unk>	С	225	<unk></unk>	50.46	31/12/1899 00:00:00
SK58588408	97.5999	<unk></unk>	94.72	С	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK58588410	95.73	94.32	92.65	S	<unk></unk>	С	225	<unk></unk>	23.45	31/12/1899 00:00:00
SK58588402	97.1699	94.72	93.54	С	<unk></unk>	С	375	<unk></unk>	27.58	31/12/1899 00:00:00
SK58589308	<unk></unk>	<unk></unk>	<unk></unk>	F	<unk></unk>	С	150	<unk></unk>	0	31/12/1899 00:00:00
SK58588501	98.9	97.26	95.51	F	<unk></unk>	С	150	<unk></unk>	30.31	31/12/1899 00:00:00
SK58589312	<unk></unk>	<unk></unk>	<unk></unk>	F	<unk></unk>	С	150	<unk></unk>	0	31/12/1899 00:00:00
SK58588307	94.65	93.17	92.75	S	<unk></unk>	С	225	<unk></unk>	31.76	31/12/1899 00:00:00
SK59580402	92.194	<unk></unk>	91.838	С	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK58588406	97.86	96.22	95.65	С	<unk></unk>	С	450	<unk></unk>	143.25	31/12/1899 00:00:00
SK58588503	97.1399	95.51	93.69	F	<unk></unk>	С	150	<unk></unk>	25.76	31/12/1899 00:00:00
SK58588404	95.54	93.86	92.25	F	<unk></unk>	С	150	<unk></unk>	24.16	31/12/1899 00:00:00
SK58589310	0	<unk></unk>	<unk></unk>	F	<unk></unk>	С	150	<unk></unk>	0	31/12/1899 00:00:00
SK58589502	95.51	94.4	94.3	S	<unk></unk>	С	150	<unk></unk>	154.2	31/12/1899 00:00:00
SK58589404	93.4199	90.84	90.69	С	<unk></unk>	С	500	<unk></unk>	195.87	31/12/1899 00:00:00
SK58588308	94.72	92.92	92.25	F	<unk></unk>	С	150	<unk></unk>	65.07	31/12/1899 00:00:00
SK58588304	97.68	95.83	93.92	S	<unk></unk>	С	150	<unk></unk>	17.1	31/12/1899 00:00:00
SK58588405	97.5999	95.65	94.72	С	<unk></unk>	С	375	<unk></unk>	21.55	31/12/1899 00:00:00
SK58588405	97.5999	95.73	<unk></unk>	С	<unk></unk>	С	375	<unk></unk>	0	31/12/1899 00:00:00
SK58589407	95.8799	94.28	90.75	С	<unk></unk>	С	150	<unk></unk>	25.56	31/12/1899 00:00:00
SK58589405	93.4199	92.24	91.47	S	<unk></unk>	С	225	<unk></unk>	58.21	31/12/1899 00:00:00
SK58588401	96.11	93.54	90.84	С	<unk></unk>	С	375	<unk></unk>	25.13	31/12/1899 00:00:00
SK58589408	95.8799	94.6	92.24	S	<unk></unk>	С	225	<unk></unk>	26.48	31/12/1899 00:00:00
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Ø	Scalaway	•	Foul Single Manhole
	Overflow	•	Combined Single Manhole
Fitting		0	Surface Water Single Manhole
	Blind Shaft	•	Twin Manhole
$\boxtimes$	Facility Connector	•	Foul Adopted Manhole
.0	Head Node	•	Combined Adopted Manhole
	Lamphole	0	Surface Adopted Manhole
•	Severage Air Value	•	Transferred Manhole
-	Severage Chemical Injection Point	•	Unsurveyed Manhole
	Severage Hatch Box	Operat	tional Site
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CI	- CAST IRON	FV	- FLAP VALVE
co	- CONCRETE	BD	- BACK DROP
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CSU	- CONCRETE SEGMENTS (UNBOLTED)	D	- HIGHWAY D
DI	- DUCTILE IRON	51	04 - SECTION 1
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MAR	- MASONRY RANDOMLY COURSED	С	- CIRCULAR
PE	- POLYETHLENE	E	- EGG SHAPED
PF	- PITCH	0	- OTHER
PP	- POLYPROPYLENE	R	- RECTANGLE
PSC	- PLASTIC STEEL COMPOSITE	S	- SQUARE
PVC	- POLYVINYL CHLORIDE	т	- TRAPEZOIDA
RPM	- REINFORCED PLASTIC MATRIX	U	- UNKNOWN
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DB - DAMBOARD

SE - SIDE ENTRY

W - WEIR

S - SURFACE WATER reserved. SEVERN TRENT

Severn Trent Water Limited Asset Data Management PO Box 5344 Coventry CV3 9FT Telephone: 0345 601 6616

# **SEWER RECORD (Tabular)**

1ap Scale: 1:2,500

This map is centred upon:

Y: 358577.67

of Issue: 04-05-20

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X: 459054.96

3 On 1 October 2011 most private severs and private lateral drains in Severn Trent Water's severage area, which were connected to a public sever as at 1 July 2011, transferred to the ownership of Severn Trent Water and became public severs and public lateral drains. A further transfer takes place on 1 October 2012, Private pumping stations, which form part of these severs or lateral drains, will transfer to ownership of Severn Trent Water on on before 1 October 2016. Severn Trent Water on the before 1 October 2016. Severn Trent Water does not posses complete records of these assets. These assets may not be displayed on the map.

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# SUPPLEMENTARY GUIDANCE NOTES RELATING TO DISPOSAL OF SURFACE WATER



# Introduction

The purpose of this guidance note is to provide advice to applicants when completing the surface water drainage design for a new development, both for Greenfield and Brownfield sites. This does not affect foul drainage disposal which should be discussed with Severn Trent as early as possible to ensure additional flows can be accommodated without undue delay to the development.

# Lead Local Flood Authority (LLFA) Consultation

Since April 2015, the LLFA have assumed the role of being a statutory consultee in the planning process for developments of 10 dwellings or more; or equivalent non-residential and/or mixed development. The LLFAs role is vital to ensure that surface water disposal on new development is adequately assessed so that the local planning authority can satisfy themselves that drainage proposals are satisfactory and to make sure, through the use of planning conditions or planning obligations, that there are clear arrangements in place for future maintenance of sustainable drainage systems (SuDS) over the lifetime of the development. This will also ensure surface water disposal aligns with local planning policies, flood risk strategies and national policies, such as the National Planning Policy Framework (NPPF).

It is strongly recommend that the LLFA are involved in early pre-application discussions when the development of a site is initially being considered. Pre-application discussions will help to ensure that SuDS are appropriately considered ahead of or as part of preliminary development layouts, and that they are fully integrated into the final development layout. Whilst Severn Trent are willing to advise on sewerage availability this does to negate the planning requirement relating to adequacy of SuDS on new development.

# **SuDS Hierarchy**

Severn Trent is fully supportive of the fundamental SuDS principle that priority should be given to managing surface water as close to source as possible. In accordance with national standards and guidance a sequential series of checks should be undertaken to ensure the relevant SuDS features are being proposed whereby (in order of priority) rainwater re-use, infiltration to ground and controlled discharge to a water body are properly considered ahead of any <u>controlled</u> connection to a culverted watercourse/other drainage system or public surface water sewer.

A controlled connection to a public combined/foul sewer would only be considered under rare exceptional circumstances where all other options have been completely exhausted. Acceptance of surface water into a combined sewer is not only unsustainable because of the need to convey/treat rainwater but is also takes away existing capacity which could constraint the connection of foul flows on future development. It is also possible that connection of additional surface water flows will require capacity upgrades to the existing sewerage system which may delay development.

# **Connection to a Public Sewer**

Whilst Severn Trent will be able to provide advice on potential public surface water sewer connection options, it is essential that a developer contacts the LLFA as early as possible to discuss surface water disposal as they will be able to provide guidance on surface water flood risk policy which may influence SuDS requirements. It is strongly recommended that LLFA discussions take place <u>before</u> contacting Severn Trent. Where the outcome of LLFA discussions concludes that a controlled discharge to the public sewerage system is the only viable option then Severn Trent would be pleased to discuss sewer connection options, satisfied that the LLFA have been consulted in line with their surface water management role and in their capacity as statutory consultee.

Evidence must be provided to demonstrate why the sequential SuDS checks have concluded that a connection to the public sewer is required. This must include a Site Investigation Report including percolation test data/graphs/calculations/results together with relevant correspondence with the LLFA.

# **Design Standards**

Surface water disposal design should consider the interactions between the adoptable sewer design criteria based on a 30 year design storm (outlined in 'Sewers For Adoption') and the "Non-statutory technical standards for SuDS" requirement to restrict discharge from a site up to and including the 1 in 100 year critical storm event plus an allowance for climate change as required by the LLFA.

For Greenfield development, the peak runoff rate should never exceed the peak pre-development run-off rates/volumes for the same rainfall event irrespective of the design storm duration consistent with the national non-statutory technical standards. For developments which were previously developed (Brownfield), the peak runoff rate must be as close as reasonably practicable to the greenfield runoff rate from the development for the same rainfall event, but should never exceed the rate of discharge from the development prior to redevelopment again for the same rainfall event. This requirement to remove pre-development surface water discharges to the sewerage system will help remove capacity constraints and aid future development.

To establish the pre-development run-off rates a detailed existing drainage survey will be required indicating pipe locations including sizes and levels, impermeable area connectivity to each pipe and topographical information to support existing drainage assumptions. Photographs of the existing buildings and surface features should be provided and where necessary a CCTV sewer survey should be provided to support the drainage survey to demonstrate connectivity.

In line with 'Sewers for Adoption', the drainage system must be designed so that, unless an area is designated to hold and/or convey water as part of the design, flooding does not occur on any part of the site for a 1 in 30 year rainfall event. For higher storm return periods the drainage system must be designed so that, unless an area is designated to hold and/or convey water as part of the design, flooding does not occur during a 1 in 100 year rainfall event in any part of: a building (including a basement); or in any utility plant susceptible to water (e.g. pumping station, electricity substation, water booster station) within the development.

# **Small Developments**

Whilst developments of fewer than 10 dwellings (or their equivalent) are excluded from the post April 2015 planning requirements the underlying principles regarding sustainable surface water management are still valid. The collective impacts of surface water discharges from smaller developments can have an adverse impact on flood risk, especially in smaller rural catchments where smaller sewerage systems are more susceptible to increases in surface water inflow. On small developments infiltration to ground and peak flow attenuation must be considered to mitigate flood risk in the community but where a sewer connection is envisaged then the developer is recommended to discuss surface water disposal options with Severn Trent as early as possible.

# Contact

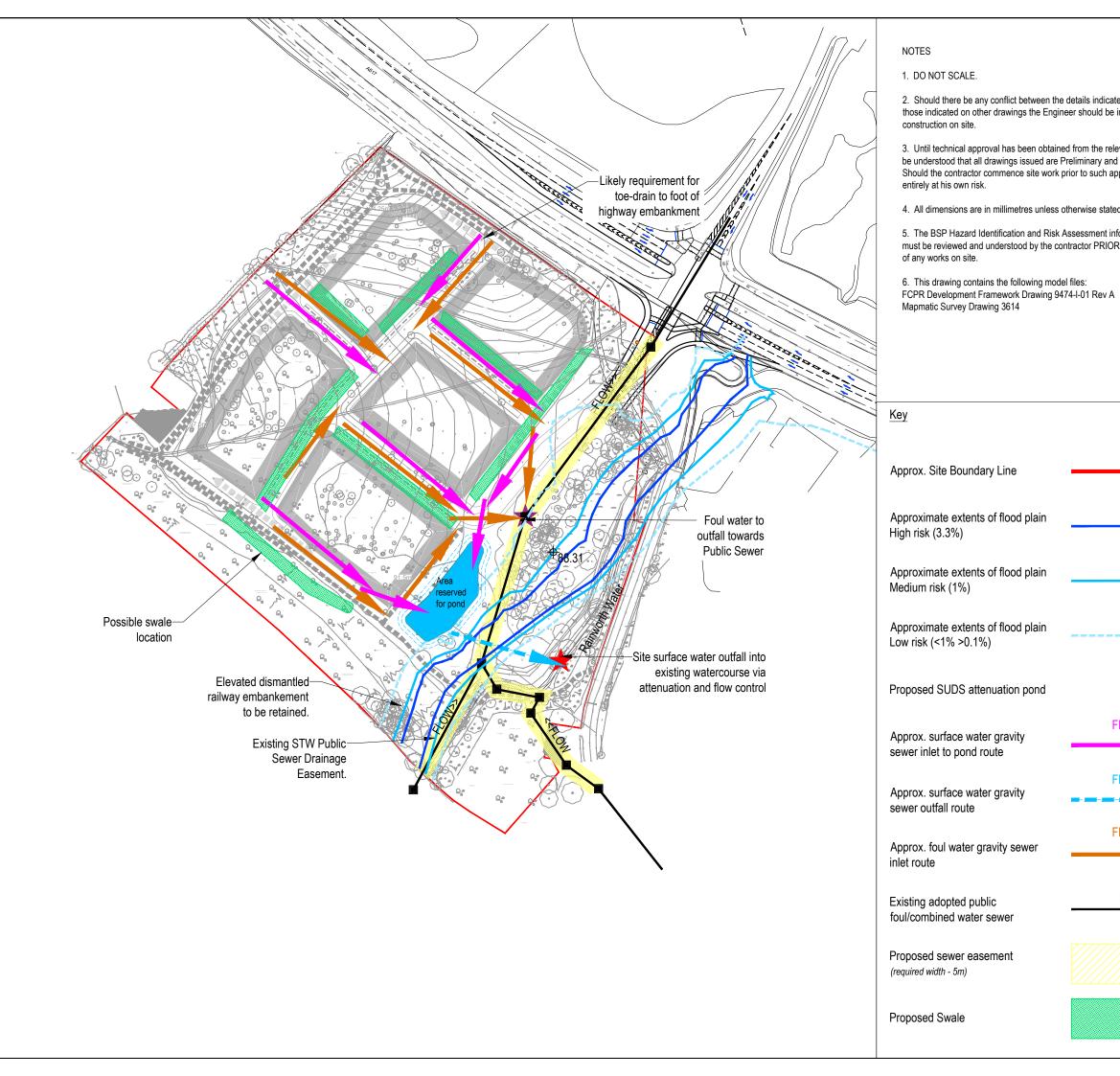
For further assistance please contact our Asset Protection teams via: <u>net.dev.west@severntrent.co.uk</u> (Birmingham & Black Country, Staffordshire, Shropshire, Worcestershire, Gloucestershire, Herefordshire, Powys) <u>net.dev.east@severntrent.co.uk</u>

(Derbyshire, Leicestershire, Nottinghamshire, Warwickshire, Coventry)



# Appendix E

Proposed Drainage Parameters RAIN-BSP-ZZ-ZZ-DR-C-0001\_P01



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# Appendix F

Qbar Greenfield Runoff Estimate



**Runoff estimation approach** 

Ben Seamer

Rainworth

Land South of A617

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and

the basis for setting consents for the drainage of surface water runoff from sites.

the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may

Calculated by:

Site name:

be

Site location:

# Greenfield runoff rate estimation for sites

www.uksuds.com | Greenfield runoff tool

# Site Details

Latitude:	53.12151° N
Longitude:	1.11912° W
Reference:	2623038802
Date:	Dec 14 2020 16:24

Runom estimation app	IH124						
Site characteristics				Notes			
Total site area (ha):	Total site area (ha):			(1) Is Q <sub>BAR</sub> < 2.0 I/s/ha?			
Methodology							
Q <sub>BAR</sub> estimation method:	rom SPR and	I SAAR	When $Q_{BAR}$ is < 2.0 l/s/ha then limiting discharge rates are set a 2.0 l/s/ha.				
PR estimation method: Calculate fro		rom SOIL typ	e				
Soil characteristics		Default	Edited				
SOIL type:		1	4	(2) Are flow rates < 5.0 l/s?			
HOST class:		N/A	N/A	Where flow rates are less than 5.0 l/s consent for discharge is			
SPR/SPRHOST:		0.1	0.47	usually set at 5.0 l/s if blockage from vegetation and other			
Hydrological characte	ristics	Default	Edited	materials is possible. Lower consent flow rates may be set whe the blockage risk is addressed by using appropriate drainage elements.			
SAAR (mm):		693	693	(3) Is SPR/SPRHOST ≤ 0.3?			
Hydrological region:		4	4				
Growth curve factor 1 year:		0.83	0.83	Where groundwater levels are low enough the use of soakaways			
Growth curve factor 30 year	rs:	2	2	to avoid discharge offsite would normally be preferred for disposal of surface water runoff.			
Growth curve factor 100 yea	ars:	2.57	2.57	)   ·			
Growth curve factor 200 yea	ars:	3.04	3.04	ĵ [			

# Greenfield runoff rates

	Default	Edited
Q <sub>BAR</sub> (I/s):	1.1	31.49
1 in 1 year (l/s):	0.91	26.14
1 in 30 years (l/s):	2.19	62.98
1 in 100 year (l/s):	2.82	80.93
1 in 200 years (I/s):	3.33	95.73

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.



# Appendix G

Mircrodrainage Quick Storage Estimate

Lange L	Variables										
Vicro	FSR Rainfal	I`		~	Cv (Summer)	0.750					
Drainage	Return Perio	d (years)	100		Cv (Winter)	0.840					
Variables	Region	England and	Wales	~	Impermeable Area (ha)	2.640					
Results	Мар	M5-60 (mm)	20.000		Maximum Allowable Discharge (I/s)	12.6					
Design	- 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	Ratio R	0.400		Infiltration Coefficient (m/hr)	0.00000					
SEC.	1				Safety Factor	2.0					
Overview 2D					Climate Change (%)	40					
Overview 3D											
Vt											
					Analyse OK	Cancel	Help				

# 18-0494 Land South of A617- Rainworth Quick Storage Estimates

Micro Drainage	Results         Global Variables require approximate storage of between 1711 m³ and 2300 m³.         These values are estimates only and should not be used for design purposes.	
Variables	- These rades are eximates only and should not be used for design purposes.	
Results		
Design		
Overview 2D		
Overview 3D	-	
Vt	-	
	Analyse OK Cancel Help	



# Nottingham

12 Oxford Street Nottingham NG1 5BG

0115 704 3300

3300 01332 374 880

Derby

Pride Park Derby DE24 8BX

5 Pride Point Drive

www.bsp-consulting.co.uk 💓 in

# Leicester

Floor 4 24 De Montfort St Leicester LE1 7GB 0116 204 7766

## Sheffield

Smithy Wood House Smithy Wood Cres Sheffield S8 0NU 0114 272 1589













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